Ultra-wide angle lens design with relative illumination analysis

W.-S. Sun
Department of Optics and Photonics, National Central University, Chung-Li 32001, Taiwan

C.-L. Tien
c1tien@fcu.edu.tw
Department of Electrical Engineering, Feng Chia University, Taichung 40724, Taiwan

Y.-H. Chen
Department of Optics and Photonics, National Central University, Chung-Li 32001, Taiwan

P.-Y. Chu
Department of Optics and Photonics, National Central University, Chung-Li 32001, Taiwan

An ultra-wide angle lens design with relative illumination analysis is presented. The half field angle of 80°, the relative illumination of the image plane will be reduced. It is necessary to increase the image numerical aperture ratio for X and Y direction, and decrease the angle between the chief ray and optical axis in the image space. However the ultra-wide angle lens induces great barrel distortion causing image extrusion. Therefore, we use F-theta distortion to replace optical distortion. Seven lenses and two pieces of flat glass are used for a sensor 1/6" sensor with 2.1 million pixels. The final result for the lens is a half viewing angle of 80°, F/2.4, a focal length 1.1 mm, a length of 22.37 mm, F-theta distortion of less than 2%, and relative illumination greater than 83%.

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1 INTRODUCTION

Generally, optical lenses with half field angle greater than 60° are called ultra-wide angle lenses. In the fisheye lenses half field angle is equal to or exceeds 90° called. In 1919 R. W. Wood [1] used a pinhole in front of a container filled with water as the prototype of the first ultra-wide angle lens, simulating the fisheye image in the water. Many improvements have been made to the ultra-wide angle lens design since that time. For example, in 1922 Bond [2] replaced Wood’s container filled with water with hemispherical glass lenses to achieve the same effect, but this produced large aberration. Beck [3] and Hill [4] added one or two lenses to improve on the Bonds aberration. Through continuous improvement, the current generation of ultra-wide angle lenses has been used in many places, such as: J. Y. Zheng [5] using a fisheye lens to capture the image and perform street panorama image processing. Furthermore, ultra-wide angle lenses are also using in unmanned remotely controlled vehicles [6] and in car recorder lens. A fisheye lens with broad spectrum is used for detecting the rice canopy or other plant growth scenarios [7]. W. Li [8] presented a panoramic stereo imaging system which uses a single camera coaxially combined with a fisheye lens and a convex mirror.

Ultra-wide-angle lenses have been discussed in a large number of related studies papers and give rise to numerous patents [9]–[14]. The requirements are as follows; half field angle ranging from 70° to 90°, and a number of elements ranging from 7 to 11; the overall length of the lens is from 25 mm to 40 mm, and the f number is 2.8. Design specifications used in this study include an 80° half field angle, 7 lenses with a length 22.37 mm, and F/2.4.

2 METHOD

The relative illumination and F-theta distortion must be considered in the ultra-wide angle lens design.

2.1 Relative illumination

The relative illumination is related to the NA of the image space and the cos^4 law. In order to calculate the NA value, five reference rays should be defined.

2.1.1 Definition of reference rays

Figure 1 illustrates the definition of the five reference rays (R1, R2, R3, R4, and R5) [15]. We set the light source at the −Y height of the object point on the object plane. The Z-axis is the optical axis. The ray passing through the center of the entrance pupil is defined as the chief ray R1; θ is the half field angle between the chief ray R1 and the optical axis in object space. We denote the four marginal rays R2, R3, R4, R5, which pass through the +Y, −Y, +X and −X of the entrance pupil.

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2.1.2 Calculation of the image numerical aperture

When the half field angle $\theta$ is zero, the chief ray R1 is located on the optical axis. The five reference rays from the exit pupil to the image plane are shown in Figure 2 and $\theta_1$ is the aperture angle between R2 and R1 in the image space. The aperture angles between the chief ray R1 and marginal rays (R2, R3, R4, and R5) are the same at the zero field angle. Therefore, the axial numerical aperture in the image space ($NA_0$) is defined as

$$NA_0 = n \sin \theta_1,$$

(1)

where $n$ is the refractive index of the image space.

When the half field angle $\theta$ is not zero, the numerical aperture is different in the X and Y direction. The off-axis Y direction reference rays are shown in Figure 3. Here is the chief angle between R1 and optical axis in the image space; $\theta_2$ is the aperture angle between R2 and R1 in the image space; and $\theta_3$ is the aperture angle between R3 and R1 in the image space.

Since aberrations have different influences on the angles of $\theta_2$ and $\theta_3$. We can calculate the average angle of $\theta_2$ and $\theta_3$. Thus the numerical aperture of Y direction ($NA_Y$) is given by

$$NA_Y = n \sin \frac{\theta_2 + \theta_3}{2}.$$

(2)

The directional cosines (L, M, N) of R1, R2 and R3 are different. They are R1 (L1, M1, N1), R2 (L2 M2, N2) and R3 (L3, M3, N3) respectively. The directional cosine is the unit vector, and $\theta_2$ and $\theta_3$ are calculated by Eq. (3) and (2.1.2).

$$\theta_2 = \cos^{-1} \left( \frac{L_1 L_2 + M_1 M_2 + N_1 N_2}{\sqrt{L_1^2 + M_1^2 + N_1^2} \sqrt{L_2^2 + M_2^2 + N_2^2}} \right)$$

(3)

$$\theta_3 = \cos^{-1} (L_1 L_3 + M_1 M_3 + N_1 N_3)$$

(4)

The off-axis X direction reference rays are shown in Figure 4. Here $\theta_4$ is the aperture angle between R4 and R1; $\theta_5$ is the aperture angle between R5 and R1.

Because the system is axial symmetric, the angles of $\theta_4$ and $\theta_5$ have the same magnitude. Therefore, the numerical aperture for the X direction ($NA_X$) is defined as

$$NA_X = n \sin \theta_4.$$

(5)

The direction cosine of R4 is (L4, M4, N4), and $\theta_4$ is given by

$$\theta_4 = \cos^{-1} (L_1 L_4 + M_1 M_4 + N_1 N_4)$$

(6)
2.1.3 Method for estimating the relative illumination

The illumination of the object in the image space, as proposed by Burle [16], is found as shown in Eq. (7)

\[ E_0 = E_{\text{obj}}RT_1NA_02\cos^4 \Theta, \]

where \( E_0 \) is the illumination of the image point from the incidence ray of the half field angle \( \theta \) in the object space; \( E_{\text{obj}} \) is illumination of object; \( R \) is the reflectivity of the object; \( T_1 \) is the penetration of the lens; \( NA \) is the numerical aperture of the image point from the incidence ray of the half field angle \( \theta \).

The relative illumination (RI) can be written as

\[ RI = \frac{E_0}{E_0} = \frac{(NA_0)^2 \times \cos^4 \Theta}{(NA_0)^2}, \]

where \( E_0 \) is the illumination of the center image point from the incidence ray for a half field angle of \( 0^\circ \).

When \( \theta \) becomes large, there will be large differences in its \( NA_X \) and \( NA_Y \) in the image space [17]. The relative illumination can be modified as in Eq. (9).

\[ RI = \frac{E_0}{E_0} = \frac{NA_0NA_X \times \cos^4 \Theta}{(NA_0)^2} \]

Finally, we can simplify this to obtain Eq. (10).

\[ RI(\theta) = \frac{\sin \left( \frac{\theta_2 + \theta_3}{2} \right) \sin \theta_4 \times \cos^4 \Theta}{\sin \theta_1^2} \]

It should be noted that the optimization process is performed to increase the angles of \( \theta_2, \theta_3, \) and \( \theta_4 \), respectively, and to reduce the angle of \( \Theta \).

2.2 F-theta distortion and calculation of the depth of field

The optical distortion is large and cannot be eliminated by the lens design with a large half field angle. It will cause the edge images close together and cannot be distinguished, so we use the F-theta distortion design to expand the edge images with a good recognition.

The F-\( \theta \) distortion [18] is given by

\[ F - \theta \text{distortion} = \frac{h' - h}{h} \times 100\%, \]

where \( h' \) is the real image height; and \( h \) is the ideal image height as

\[ h = f \times \theta, \]

where \( f \) is the focal length of the lens; and \( \theta \) is the half field angle for which the unit is radians.

3 DESIGN RESULTS

3.1 Specifications of sensor and lens

We use the OV2722 sensor with 2.1 million pixels. The pixel size of the sensor is 1.4 \( \mu \)m and the specification is shown in Table 1. The requirement of an ultra-wide angle lens design is shown in Table 2. In object space, a half field angle of 80\(^\circ\), F/2.4, and a focal length 1.1 mm are specified in our design.
TABLE 3 The lens data of the ultra-wide angle lens design.

<table>
<thead>
<tr>
<th>No</th>
<th>Type</th>
<th>Radius</th>
<th>Thickness</th>
<th>Glass</th>
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<td>2.00867</td>
<td>6968.5541</td>
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<tr>
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<td>3.14572</td>
<td>5292.6000</td>
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<tr>
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<td>1.8</td>
<td>7174.2962</td>
</tr>
<tr>
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<td>Asphere</td>
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<tr>
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<td>1.61405</td>
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<td>17</td>
<td>Sphere</td>
<td>infinity</td>
<td>0.53175</td>
<td>5168.6417</td>
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TABLE 4 The aspherical coefficient of the ultra-wide angle lens design.

<table>
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<tr>
<th>Surface</th>
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<th>4th order</th>
<th>6th order</th>
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<tr>
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<td>0</td>
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</tbody>
</table>

FIG. 6 MTF and spatial frequency at infinity object distance.

FIG. 7 F-θ distortion for the ultra-wide angle lens design.

FIG. 8 Lateral color for the ultra-wide angle lens design.

FIG. 9 Relative illumination for the ultra-wide angle lens design.

4 CONCLUSION

There are five spherical glass lenses and two aspheric plastic lenses and two flat glass plates in the optical system. The design result for the ultra-wide angle lens is a half field angle of 80°, F/2.4, a focal length 1.1 mm, and a total length of 22.37 mm. In the optimization process, we increase the $(NA_Y \times NA_X \times \cos^4 \Theta)/(NA_0^2)$ value so that we can achieve greater than 83% relative illumination. The F-theta distortion is less than 2% and lateral chromatic aberration is less than 1.4 μm.
5 ACKNOWLEDGEMENTS

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References