Guided-mode triggered switching between TE orders of a metal-based grating-waveguide

O. Parriaux

Hubert Curien Laboratory UMR CNRS 5516, University of Lyon, 42000 Saint-Etienne, France

An undulated metal-based dielectric slab waveguide is shown to exhibit a high contrast broadband switching effect in the angular spectrum between the oth order Fresnel reflection and the propagating -1^{st} reflected diffraction orders. The switching trigger is the synchronous collinear coupling of an incident TE plane wave to the close-to-cutoff forward- and backward-propagating fundamental TE₀ mode of the waveguide via the $+1^{st}$ and -2^{nd} order of the periodic undulation.

[DOI: http://dx.doi.org/10.2971/jeos.2015.15040]

Keywords: Optical diffraction, optical gratings, optical switching, optical waveguides

1 INTRODUCTION

It is known that a sinusoidal metal grating exhibits a close to 100% diffraction efficiency under the -1st order Littrow incidence with a cancellation of the Fresnel reflection at a definite grating depth [1]; the depth at which the 0th order cancellation occurs is smaller for the TM than for the TE polarization. The diffraction efficiency increases monotonically versus the depth, then oscillates periodically with a decrease of the -1st order efficiency maximum due to increasing metal losses. The angular range of maximum -1st order around the Littrow angle $\theta_L = \sin^{-1}(\lambda/(2\Lambda))$ (λ is the wavelength in vacuum, Λ the grating period) is usually very broad and is limited by the higher reflected orders starting to propagate. It was shown recently [2] that the situation changes radically for the TM polarization if the -2nd or +1st order of the grating couples to the forward, resp. backward surface plasmon in which case the efficiency of the propagating -1st order experiences a sharp drop to 0 at either side of the Littrow angle where the 0th order Fresnel reflection angular spectrum peaks at a close to 100% maximum [2]. The condition for this high contrast plasmon-mediated switching to take place within a definite angular band around the Littrow angle is $3 K_g (= 3(2\pi/\Lambda))$ only slightly larger than twice the plasmon propagation constant $2\beta = 2n_e k_0$ (n_e is the surface plasmon effective index and $k_0 = 2\pi/\lambda$; this prevents higher order diffracted waves to propagate. One remarkable feature of this high contrast switching effect in the angular domain between propagating orders is that it is extremely low-loss although mediated by resonant plasmon coupling. The reason for such low-loss plasmonic mechanism was elucidated by a coupledmode analysis [3] which showed that the coupled forwardand backward-propagating plasmon fields re-radiate much before being absorbed into the incident medium along the propagating 0th and -1st order directions where high contrast constructive or destructive interference takes place depending on the relative phase of the re-radiated fields.

Whether such high contrast triggered switching effect can also

exist in the angular spectrum for an incident TE wave is unknown, and difficult to imagine since no surface plasmon can be excited. The present work reports on the search for, and the discovery of a new switching effect for the TE polarization with the mediation of a dielectric-waveguide mode in place of the plasmon mode.

2 FROM PLASMON- TO WAVEGUIDE-MODE TRIGGER

Whereas the sinusoidal metallic grating generating the propagating -1st reflected order inherently also couples the incident wave to the co- and contra-propagating plasmon modes upon an angular tilt in the incidence plane [2], there is no such resonance in the same structure for the TE polarization. Triggering such switching effect for the TE polarization requires the existence of a TE-resonance. This resonance can be a mode of a dielectric layer of refractive index n_{g} and thickness w also coupled by a grating. However, the TE trigger can not consist of a sole dielectric waveguide on a dielectric substrate because there would be propagating orders into the substrate as well since the 0th and -1st orders propagate in the lower refractive index incident medium (air in the present case). As a result it would be impossible to achieve a high contrast constructive or destructive interference condition in the directions of the 0th and -1st orders in the cover medium unlike in the plasmonic case where the sole 0th and -1st orders propagate [3]. Consequently, the dielectric waveguiding layer must have a metallic substrate very much like the plasmonic structure as illustrated in Figure 1.

In analogy to the plasmon-triggered TM switching [2], the plasmon mode is now replaced by the fundamental TE₀ mode which the grating couples either in the backward direction via its -2^{nd} order when the incidence angle θ_{-2} is smaller than the -1^{st} order Littrow angle or via its $+1^{st}$ order when θ_1 is larger

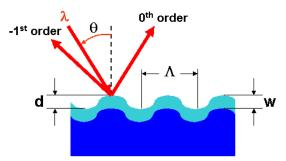


FIG. 1 Dielectric waveguiding layer of index n_g and thickness w conformally deposited on a sinusoidal metal grating of period Λ and depth d with TE incidence at wavelength λ under the angle θ and the sole oth and -1st reflected orders propagating in the incidence medium.

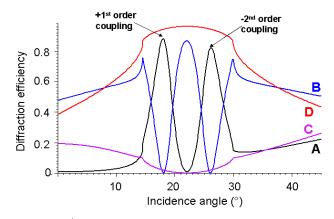


FIG. 2 -1st and oth order angular spectra summarizing the design process of the TE₀ waveguide-mode-triggered switch, $\lambda = 633$ nm, $\Lambda = 844$ nm, undulated silver substrate of complex permittivity $\epsilon_m = -16.1 + i1.1$. Curves C and D: optimized sinusoidal grating depth d = 320 nm in a silver substrate without dielectric layer achieving maximum -1st order diffraction efficiency and cancellation of the oth order under the Littrow mount at 22 degree incidence. Curves A and B: optimized grating depth d = 240 nm and waveguide thickness w = 180 nm ($n_g = 1.46$) achieving high contrast oth to -1st order switching with cancellation of the -1st order at the mode coupling angles.

than the Littrow angle θ_L . The corresponding phase matching conditions are, respectively:

$$k_0 \sin \theta_{-2} + k_0 n_e = 2K_g \tag{1}$$

and

$$k_0 \sin \theta_1 + K_g = k_0 n_e \tag{2}$$

where K_g is the grating constant $2\pi/\Lambda$ corresponding to the Littrow angle θ_L at the wavelength λ .

3 GENERAL DESIGN AND PROPERTIES

The design process starts by finding numerically the depth of a sinusoidal grating at a silver surface at which the TE 0th order cancels and the -1st order is maximum under the Littrow condition. The considered optogeometrical parameters are the same as those of the plasmonic structure [2] to permit a comparison of the optical function: 22 degree incidence and $\lambda/\Lambda = 633/844$ nm/nm = 0.75 with air overlay in the absence of dielectric layer; the metal is silver too. Curves C and D in Figure 2 represent the 0th and -1st order spectra obtained with a grating depth d = 320 nm; the two kinks at 14.5 and 30 degrees on these two smooth curves represent the cutoffs of the

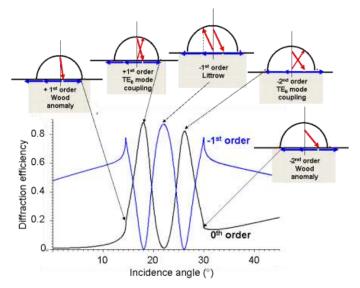


FIG. 3 Waveguide-mode triggered switching between the oth and -1^{st} TE orders in the angular spectrum centered on the -1^{st} order Littrow mount at 22 degree incidence with all features illustrated in the Ewald circles in which the blue vectors represent the grating constant K_g , the red spots the propagation constant β of the waveguide mode, and the red arrows the wave vectors of the incident and oth and -1^{st} order diffracted waves. The considered optogeometrical parameters are those of Figure 2, curves A and B.

+1st and -2nd diffraction orders respectively. The sinusoidal metal undulation is now coated with a conformal dielectric layer; similarly to the plasmon-triggered structure [2, 3] the grating depth is then varied to find out whether a cancellation of the -1st order amplitude at either side of, and close to the Littrow angle can also be obtained; the -1st and 0th order spectra B and A of Figure 2 show that it is the case indeed: a grating depth of 240 nm for a 180 nm thick dielectric layer of 1.46 index n_g do lead to a cancellation of the -1st order and a peak of the Fresnel reflection.

It is at the angles θ_{-2} and θ_1 of synchronous TE₀ mode coupling as given by expressions (1) and (2) that the 0th order Fresnel reflection reaches its maximum, and zero at the Littrow angle θ_L , once the grating depth is adjusted so as to give rise to constructive or destructive interference in the incident medium (here air) in the directions of the 0th and -1^{st} orders. For the diffraction process to involve the -2^{nd} , -1^{st} , 0th and $+1^{st}$ orders only, and to have them to operate within the angular width of the -1^{st} order Littrow condition $2\lambda/\Lambda - 1 < \sin \theta < 1 - \lambda/\Lambda$ between the cutoffs of the -2^{nd} and $+1^{st}$ orders, the propagation constant β of the TE₀ mode must be very small, i.e., the mode must be close to its cutoff (n_e close to 1 in the considered case of air incident medium whatever the refractive index n_g of the dielectric waveguide layer).

Figure 3 represents synthetically in the reciprocal space the relationship between all involved spatial frequency vectors in the Ewald circle at the specific features of the angular spectra. The considered structure is that leading to the -1st and 0th order spectra B and A of Figure 2.

Unlike in the TM case where the plasmon effective index is essentially determined by the metal permittivity [2] – and to a

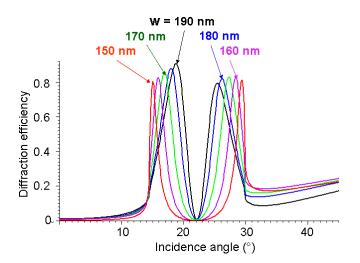


FIG. 4 Tailoring of the angular spectral width of the oth to -1st order switching by changing the thickness of the dielectric layer of refractive index $n_g = 1.46$ with w as a parameter. The oth order spectrum only is represented. The corresponding effective index of the TE₀ mode with increasing thickness is 1.010, 1.024, 1.042, 1.06, 1.072.

much lesser extent by the grating depth – the effective index of the TE₀ mode of the dielectric layer is strongly dependent of the dielectric layer thickness w. This means, as illustrated in Figure 4, that the angular distance between 0th and -1st order maxima can be adjusted by the layer thickness w. It is noteworthy that all 5 spectra have quasi-zero 0th order at the Littrow angle for the same grating depth of 240 nm. Worth noting also is the fact that the absorption loss (between 10 and 20% as the complement to 1 of the diffraction efficiency maxima) is comparable with the absorption loss of the plasmon-triggered switch [2].

Setting the incidence angles θ_1 and θ_{-2} within the Littrow angular width at which the maxima of the 0th order is desired determines the needed effective index n_e from the conditions in Eq. (1) or Eq. (2). Inserting the desired ne into the dispersion equation of a dielectric slab waveguide TE₀ mode [4] with air superstrate and metal substrate of real part of negative permittivity ϵ_{mr} yields the thickness w of the needed waveguide layer:

$$w = \frac{\left(\tan^{-1}\left(\sqrt{\frac{n_{e}^{2} - \epsilon_{mr}}{n_{g}^{2} - n_{e}^{2}}}\right) + \tan^{-1}\left(\sqrt{\frac{n_{e}^{2} - 1}{n_{g}^{2} - n_{e}^{2}}}\right)\right)}{k_{0}\sqrt{n_{g}^{2} - n_{e}^{2}}}$$
(3)

Introducing *w* obtained from Eq. (3) into an exact code calculating the diffraction of the undulated metal substrate loaded with a dielectric layer of uniform thickness *w* using the Chandezon method [5] will however not give the 0th order maximum exactly where it was desired at θ_1 and θ_{-2} because dispersion equation (Eq. (3)) is for a planar metal-based waveguide structure without undulation. The fact that the dielectric waveguide is undulated decreases slightly the effective index; however, the provided *w* is a safe departure point for a numerical optimization. Besides, under the hypothesis of a close-to-cutoff TE₀ mode, the transcendental dispersion equation (Eq. (3)) can be explicitly solved for the effective index n_e after some algebraic approximations using the fact that n_e is very close to 1:



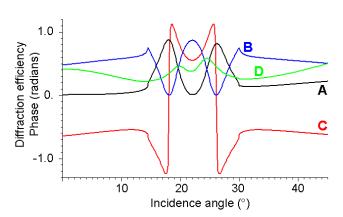


FIG. 5 Phase spectrum in radians of the fields of the -1^{st} order (curve C) corresponding to the structure of Figure 2 (curves A and B). The green curve D is the o^{th} order spectrum of the TM polarization in the same structure.

where

$$\delta = \frac{n_g^2 - 1}{2} \left[\frac{\pi}{2} - \sqrt{n_g^2 - 1} \left(k_0 w + \frac{1}{\sqrt{1 - \epsilon_{mr}}} \right) \right]^2$$

The evidence that the cancellation of the -1^{st} order and maxima of the 0^{th} order occur under the condition of a TE mode excitation is given in Figure 5 which shows, in addition to the 0^{th} and -1^{st} order spectra used in Figure 2, the phase profile of the -1^{st} order field: there is a large and sudden phase jump of 2.4 radians characteristic of mode excitation at the angular position of the two 0^{th} order maxima.

Interestingly, calculating the TM angular spectrum of the 0th order (curve D) of the very same structure (curves A and B) shows that obviously the contrast is poor since the structure is not designed for the plasmon-triggered switching, but reveals that the 0th order maxima are notably closer to each other than in the TE spectra which means that the effective index of the TM₀ mode is larger than the TE₀'s; the reason for this lies on the fact that the substrate is metallic, therefore the fundamental mode is of plasmonic nature (the field in the dielectric waveguide is evanescent) and its effective index is as large as 1.51.

An important comment must be made at this stage about the phenomenology of the designed waveguide-mode mediated switching effect: the coupled-mode interpretation of the TM plasmon-mediated switch [3] reveals that the astonishingly low-loss plasmonic effect and its high interference contrast originate in the plasmon radiation strength of the rather deep grating being notably larger than the absorption coefficient of the plasmon mode. Although the coupled-mode analysis of the present TE switch hasn't been developed, the same rationale can be applied: the TE₀ waveguide mode coupled by the +1st and -2nd orders of the grating is radiated back to the incident medium along the 0^{th} and -1^{st} order directions before being absorbed by the metallic substrate. A sign of this is the fact that the direct -1st order excitation of the TE₀ mode in the same structure exhibits a loss of about 70% (99% at a grating depth of 50 nm) whereas the loss associated with the +1st and -2nd order coupling (see Figure 2) is about 15 and 20% only.

The design process and all examples above use as a model a dielectric layer of 1.46 refractive index n_g . This is by no means

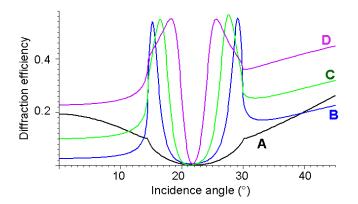


FIG. 6 Reflected oth order TE angular spectra with Λ = 844 nm, λ = 633 nm, n_g = 2.4. A: No dielectric layer, d = 320 nm. B: w = 60 nm, d = 230 nm, n_e = 1.077. C: w = 62 nm, d = 200 nm, n_e = 1.100. D: w = 64 nm, d = 170 nm, n_e = 1.130.

a restriction since it is the effective index of the TE₀ mode that essentially matters. As an evidence of this, Figure 6 is the analogue of Figure 4 with a waveguide layer of refractive index $n_g = 2.4$ which may approximately correspond to a ZnS, TiO₂ or diamond layer in the visible and near infrared domains. In the presence of a high index layer the waveguide thickness *w* must be adjusted (i.e., decreased) to give rise to an effective index n_e of the TE₀ mode sufficiently close to its cutoff (i.e., close to 1 here). The angular spectra (the 0th order Fresnel reflection only is shown in Figure 6) exhibit the same general pattern, but evidently the control over the layer thickness w is much more critical to give rise to a sufficiently small effective index. Curves B, C and D of Figure 6 show here too, as in Figure 4, a feature which the plasmon-triggered switch does not exhibit: changing the waveguide thickness *w* permits to vary the angular distance between 0th and -1st order maxima/minima, i.e., the operation range of the switch. Using a high index dielectric layer is however not so interesting practically since the 0th order remains large outside the angular switching range and the absorption loss is slightly larger.

4 CONCLUSION

The present analysis shows that the plasmon-triggered switching effect between two free-space orders first reported in [2] and elucidated in [3] can be extended to the TE polarization by providing a resonance in the form of the fundamental TE₀ guided mode of a close-to-cutoff thin dielectric layer deposited onto a metal grating. Similarly to the plasmonmediated case, the TE switch exhibits absorption losses which are notably smaller than under direct mode coupling by the same grating. An interesting, although unexpected, common characteristic of the plasmon and dielectric mode-triggered structures lies in that the very same metal grating depth of 240 nm gives rise to the TM switching with air in the grooves and to the TE switching with a 150-190 nm thick dielectric layer of index 1.46 covering the sinusoidal corrugation. The specific interest of the TE switch is to enable the angular distance between 0th order maxima to be adjusted by controlling the waveguide thickness. The present analysis was made assuming a conformal dielectric film deposited onto an undulated metal substrate; this condition would not be fulfilled with a spin-coated dielectric film (polymer or Sol-Gel waveguide), that is why vacuum deposition technologies like PVD Physical Vapour Deposition, (PE)CVD (Plasma Enhanced) Chemical Vapour Deposition, or ALD Atomic Layer Deposition should be used to satisfy this assumption.

This surface-wave-triggered switching effect can be used in the field of security and anti-counterfeit applications where angular tilting is often used. It could also be used to separate or combine two broad wavelength spectra at fixed incidence angle by exploiting the waveguide dispersion characteristics.

References

- E. Popov, L. Tsonev, and D. Maystre, "Gratings General properties of the Littrow mounting and energy flow distribution," J. Modern Optics 37, 367–377 (1990).
- [2] J. Sauvage-Vincent, Y. Jourlin, V. Petiton, A. V. Tishchenko, I. Verrier, and O. Parriaux, "Low-loss plasmon-triggered switching between reflected free-space diffraction orders," Opt. Express 22, 13314–13321 (2014).
- [3] A. V. Tishchenko, and O. Parriaux, "Coupled-mode analysis of the low-loss plasmon-triggered switching between the oth and -1st orders of a metal grating," IEEE Photon. J. (2015) article in press.
- [4] P. K. Thien, "Light waves in thin films and integrated optics," Appl. Optics 10, 2395-2413 (1971).
- [5] N. Lyndin, MC Grating Software, http://www.mcgrating.com/